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Exploratory Review of Reinforcing Solutions for Precast Concrete 3-D Printing

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ABSTRACT

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There is a lack of knowledge for reinforcing methods in the cutting-edge technology of Precast Concrete 3-D Printing (PCP). This study explores reinforcing solutions and their implementations in PCP members. Two solutions are proposed to be applied in PCP: 1) Post-tensioning tendons & 2) Steel-fiber orienting method. A literature review of the relevant technologies and the implementation procedures of the reinforced 3-D printed precast concrete concept is presented in this research. The literature topics investigated in this study include precast concrete 3-D printing, mix design of concrete 3-D printing, types of fibers used in concrete and methods for orienting fibers, and post-tensioning method. Traditionally, Fiber-Reinforced Concrete (FRC) contains discrete fibers that are uniformly distributed and randomly oriented. Previous research has shown that the manipulation of the fiber dispersion and orientation to match the stress field pattern is significantly influential on the mechanical behaviors of FRC. Implementation of this concept leads to print the fibers in the stress trajectory of precast concrete members. This concept is explored in this study. Furthermore, the implementation procedure of post-tensioning tendons in PCP members is investigated. The theoretical framework provided in this study paves the way for the industrialization and applicability of PCP in the precast industry.

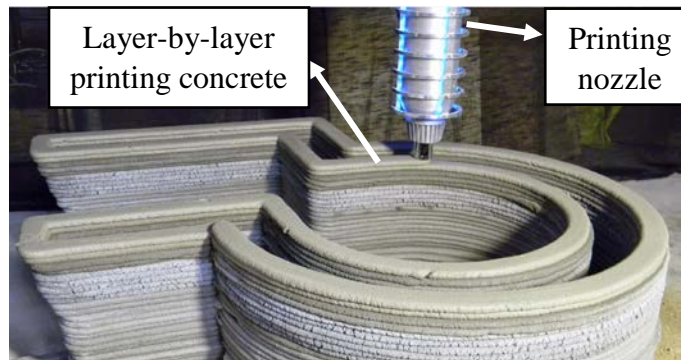
39 **Keywords:** Additive manufacturing; Buildability; Extrudability; Fiber-induced flow;
40 Intentionally oriented fibers; Post-tensioning method

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42 INTRODUCTION

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44 Up until the last decade, additive manufacturing has been exclusively used in high-tech
45 technologies such as aerospace and biomedical engineering. In recent years, there has been a
46 significant increase in the application of large-scale 3-D printing, specifically with different
47 materials such as metals¹, polymers², and concrete and cementitious materials^{3,4,5}.
48 Traditionally, concrete is cast into a formwork - typically containing a reinforcement cage -
49 and then consolidated to be used in structural components such as beams, slabs, columns, etc.
50 The 3-D printing of cementitious material facilitates the geometry of cast concrete (Fig. 1) and
51 also the shape of the formwork. Irregular formworks can be printed to help casting ordinary
52 concrete and producing any unconventional or aesthetic shapes (Fig. 2). This technology
53 improves construction projects in different ways such as accelerate the construction process,
54 implement where there is not enough manpower, and implement where a delicate/irregular
55 surface is needed.



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57 Fig. 1- Layer-by-layer concrete printing to a desired geometry (photo courtesy of 3D
58 Concrete House Printer⁶, used with permission)

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Fig. 2- A sample of printed formwork to make an aesthetic concrete surface

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63 There is a lack of knowledge about the reinforcing methods of concrete 3-D printing. The bond
64 between printed concrete and reinforcement must be present to reach the desired strength of
65 the concrete components. This is particularly difficult to perform due to the nature of the layer-
66 by-layer filament casting in concrete 3-D printing (Fig. 1). Considering the properties of
67 Precast Concrete 3-D Printing (hereafter referred to as “PCP”), the post-tensioning method can
68 be applied to resolve the concrete-to-reinforcement bonding problem. This is plausible due to
69 the characteristics of the bonded, post-tensioning method (in which grouting is used to bond
70 between concrete and post-tensioned tendons).

71 Additionally, structural behaviors of printed concrete can be improved by adding
72 supplementary materials to obviate the need for other reinforcement. One example of these
73 supplementary materials is the Fiber-Reinforcement Concrete (hereafter referred to as “FRC”).
74 FRC is a concrete mix that contains fibrous materials, which improve the concrete’s structural
75 integrity. Traditionally, FRC contains discrete fibers that are uniformly distributed and
76 randomly oriented⁷. This arbitrary dispersion of fibers leads to inefficient structural integrity
77 and strength. There exists a method for specifically orienting the fibers in concrete, which is
78 comprehensively discussed in the section “BACKGROUND”.

79 The objective of this study is to explain and explore two methods, post-tensioning and steel-
80 fiber orienting methods, that obviate the need for reinforcement in the cutting-edge precast
81 concrete 3-D printing (PCP) technology. The first method involves the application of post-
82 tensioning tendons in PCP members at the stressed locations and directions; this leads to a
83 stronger structure that compensates for the lack of reinforcement. In contrast, the method for
84 the intentional orientation of fibers in Fiber-Reinforced Concrete leads to a stronger material
85 that requires no additional reinforcement. The “casting-flow induced” method is proposed in
86 this study to orient the fibers in PCP members⁷.

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88 **BACKGROUND**

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90 **PRECAST CONCRETE 3-D PRINTING**

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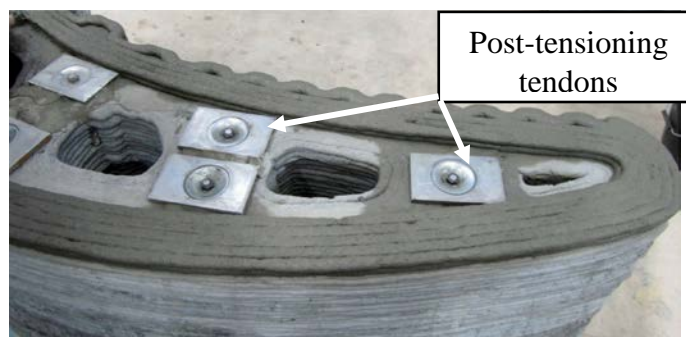
92 3-D printing is an additive and automated procedure for constructing 3-D solid objects from a
93 simulated model in the control unit. Conceptually, a series of 2-D layers is printed on top of
94 each other to build the three-dimensional simulated model⁸ (Fig. 3). Pegna initially suggested
95 and explored the concept of cementitious material 3-D printing⁹. Concrete 3-D printing was
96 initially employed to construct complex geometrical shapes without the use of formwork^{10,11}.
97 This is a significant advantage compared to conventional construction methods. Lim et al. used
98 twenty-three post-tensioning tendons on a printed concrete member only for vertical
99 reinforcement (i.e. transverse reinforcement against shear forces) as shown in Fig. 4 [5]. The
100 current study explores the possibility of longitudinal (flexure) reinforcement in addition to
101 transverse (shear) reinforcement in PCP members.

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103

104 Fig. 3- 3-D printing of concrete (photo courtesy of 3D Concrete House Printer⁶, used with
105 permission)



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107 Fig. 4- Vertical post-tensioning tendons (photo courtesy of Lim et al. (2012)⁵, used with
108 permission)

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110 MIX DESIGN OF CONCRETE 3-D PRINTING

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112 There are two main fresh properties of concrete that facilitate the PCP procedure: extrudability
 113 and buildability. These two properties are closely related to workability and the open time of
 114 fresh concrete. The mix design proportion and the presence of supplementary cementing
 115 materials (such as superplasticiser, retarder, accelerator and polypropylene fibers) affect those
 116 mentioned properties³. Extrudability is the ability to transport the printing concrete from the
 117 pumping system to the nozzle where it becomes a layer of filament¹². The open time is the
 118 period in which cementitious materials have not yet settled and the workability of the fresh
 119 concrete stays at a level that makes extrudability possible³; the open time is usually tested with
 120 a Vicat apparatus. In PCP, the buildability of fresh concrete is defined as the number of printing
 121 filament layers that can be built up without undesired deformation^{3,13}. Previous research³ has
 122 proposed that the optimum mix design for concrete 3-D printing fulfil all the mentioned
 123 requirements as shown in Table 1.

124

125 Table 1- Optimum mix design of printing concrete

Property		Quantity
Maximum aggregate size		2mm
Sand to binder ratio		3 to 2
Binder components	Cement	70%
	Fly ash	20%
	Silica fume	10%
	Polypropylene fibers	1.2 kg/m ³ of 12/0.18 mm (length/diameter)
Water to binder ratio		0.26
Notes:		
1. A 9mm diameter nozzle is deemed appropriate for printing with the mix design.		
2. In one session, this system can build 61 layers in one session without significant deformation of bottom layers.		
3. The open time of fresh concrete can be up to 100min.		
4. The compressive strength of concrete can be obtained as much as 110 MPa (16 ksi) at 28 days.		

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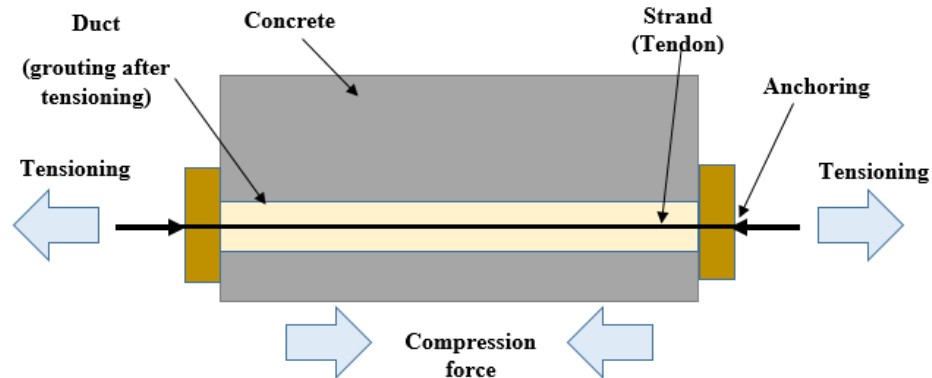
127 POST-TENSIONING METHOD IN PRECAST MEMBERS

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129 Post-tensioned concrete is a type of precast concrete member (along with prestressed concrete)
 130 in which surrounding concrete elements are initially cast and the tendons are tensioned
 131 afterwards¹⁴. However, the concrete is not placed in direct contact with tendons. The tendons
 132 are encapsulated through a protective duct or sleeve, that is either cast inside the concrete
 133 element or placed adjunct to it. Tendons at each end are then firmly fixed to the surrounding
 134 concrete. Once the concrete is fully cast and settled the tendons are stretched (tensioned) at
 135 each end and the encapsulated concrete undergoes a resultant compressive force. By grouting

136 the duct after tensioning, the tendon is bonded to the surrounding concrete; this is called
 137 “bonded post-tensioning” (Fig. 5).

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Fig. 5- Post-tensioning mechanism

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142 FIBER-REINFORCED CONCRETE AND FIBER-ORIENTING METHOD

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144 The concept of composite materials was initially considered in 1950s and FRC was one of the
 145 topics of interest in this category^{15,16}. Fiber-Reinforced Concrete (FRC) contains discrete fibers
 146 that are uniformly distributed and randomly oriented. Previous research has shown that the
 147 manipulation of the fiber dispersion and orientation to match the stress field pattern is
 148 significantly influential on the mechanical behaviors of FRC⁷. In order to orient the fibers in
 149 concrete, the “casting-flow induced” method can be used⁷. Ferrara et al. showed that by virtue
 150 of a specific concrete mix design and an appropriate casting procedure, steel-fibers can be
 151 efficiently tailored along the direction of tensile stresses. The mix design proportion of
 152 concrete that leads to “casting-flow induced” concrete is shown in Table 2. It should be noted
 153 that the magnetic method proposed by Ferrara et al. is a nondestructive technique to monitor
 154 the direction and dispersion of fibers within a structural element^{17,18}.

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Table 2- Mix design for constructing cast-flow induced FRC

Property		Quantity
Maximum aggregate size		2mm
Sand to binder ratio		1.5 to 2
Binder components*	Cement type I 52.5	50%
	Slag	42%
	Straight steel fibers**	8%
Water to binder ratio		0.17
Notes:		
* Superplasticizer used in the mix design is 33 l/m^3 .		
* Length (l_f) and diameter (d_f) of fibers are 13mm and 0.16mm, respectively.		

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166 PROPOSED REINFORCING METHODS FOR PRECAST CONCRETE 3-D 167 PRINTING

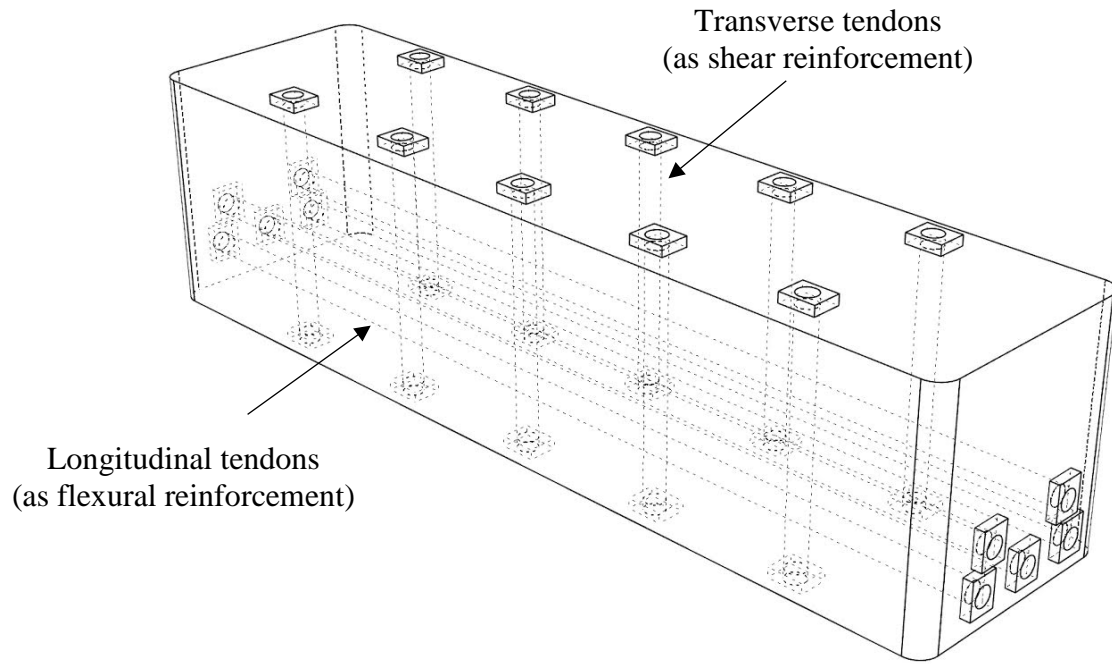
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169 In this study, two methods are proposed and explored to reinforce PCP elements, including 1)
170 post-tensioning tendon method and 2) fiber-orienting method.

171 1) Post-Tensioning Method

172 As mentioned in the section “BACKGROUND”, Lim et al.⁵ showed that the possibility of
173 transverse reinforcement in PCP members through the post-tensioning method. However, the
174 current study suggests not only the transverse post-tensioning reinforcement (against shear
175 forces) in PCP members, but also the longitudinal post-tensioning reinforcement (against
176 flexural forces), as shown in Fig. 6. In general, the bond between concrete and reinforcement
177 in PCP is difficult to achieve. The application of post-tensioning tendons could reduce (if not
178 eliminate) this difficulty by grouting the ducts after stressing (tensioning) the tendons. In
179 addition, the use of duck sleeve could be avoided by designing voids in the simulated program
180 that can be printed in layers (Fig. 6).

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a) Post-tensioning tendons



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b) PCP member

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Fig. 6- Configuration of post-tensioning method to reinforce PCP members

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A future study is recommended as the follow-up research to conduct an experimental program

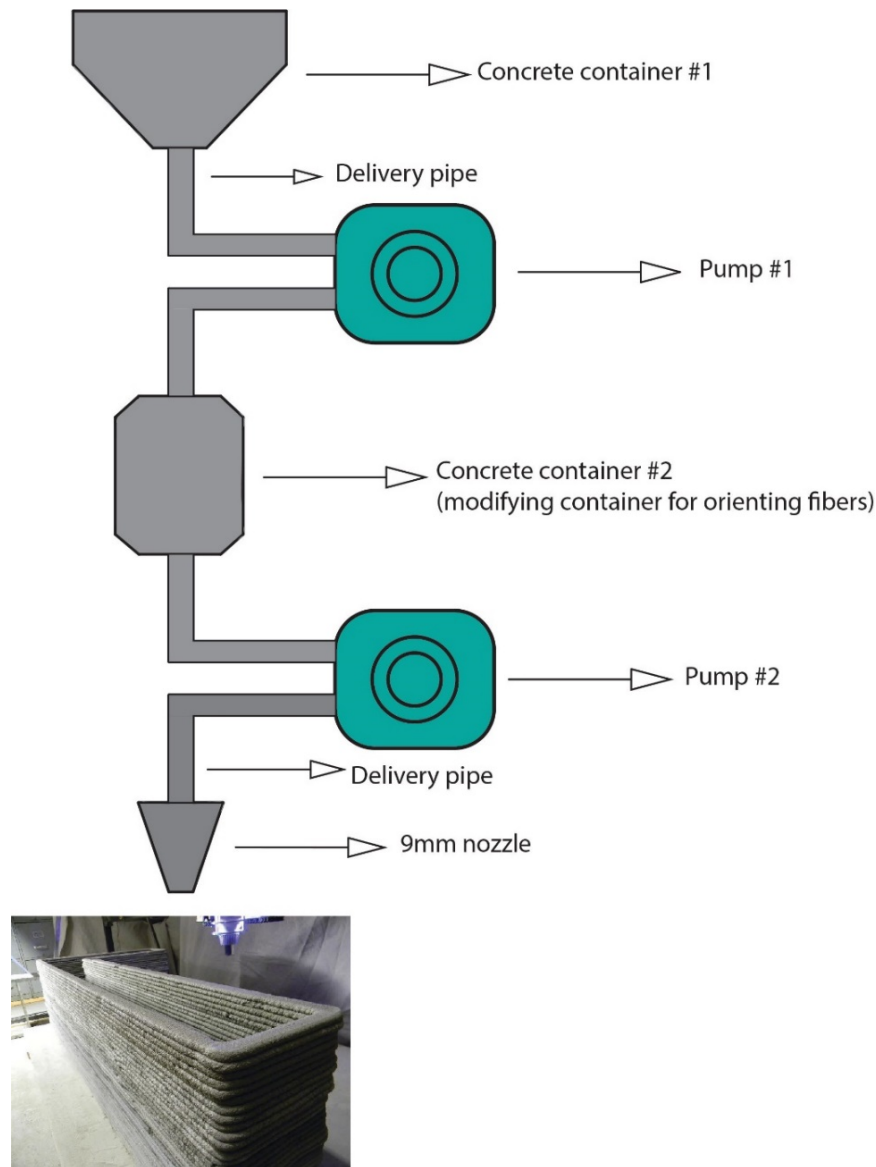
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where different variables (such as the post-tensioning tendon size, PCP cross-section and

189 length, and printing nozzle diameter) are investigated. This study would further identify the
 190 variables affecting PCP shear and flexural capacities (Fig. 6).

191 2) Fiber-Orienting Method

192 In this method, it is proposed that the concrete mix design is manipulated such that to orient
 193 fibers along with the direction of the tensile trajectory of PCP members. The optimum mix
 194 design needed for printing concrete layers (using a 9mm-diameter nozzle) is shown in Table
 195 1. In addition, Table 2 shows the optimum mix design for the implementation of reinforcing
 196 fibers. The current study proposes to combine these two mix designs through a concrete
 197 delivery system that uses two concrete containers and two pumps. Fig. 7 shows the schematic
 198 for the proposed delivery system.



199

200 Fig. 7- Schematic of the proposed concrete delivery system (after Le et al. 2012³)

201 In this proposed printing procedure, Container #1 contains the mix design presented in Table
202 1. This concrete is then pumped to Container #2, which provides the concrete with the
203 necessary reinforcing fibers needed for the fiber-orienting procedure. In this container, the
204 binder quantity is doubled by adding 50% Cement type I, 42% slag, and 8% straight steel fibers
205 (13mm long and 0.16mm diameter) to the concrete batch. Thus, the sand to binder ratio
206 becomes 1.5 to 2. Additionally, 33 l/m^3 superplasticizer is required to be added to Container
207 #2. Pump #2 is then used to push the concrete through the delivery pipes and out the 9mm-
208 diameter nozzle.

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211 SUMMARY AND CONCLUSIONS

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213 This study explored and proposed the implementation of two reinforcing methods, one
214 involving post-tensioning tendons and the other steel-fiber orienting, to the cutting-edge
215 technology of Precast Concrete 3-D Printing (PCP). The relevant technologies and their body
216 of knowledge were investigated, including concrete 3-D printing, mix design of concrete 3-D
217 printing, types of fibers used in concrete and the fiber-orienting method, and the post-
218 tensioning method. This study proposed a post-tensioning procedure to reinforce PCP
219 members against both shear and flexural forces in an effort to mimic the stirrups and
220 longitudinal reinforcement in RC members. In addition, the application of the fiber-orienting
221 method in Fiber-Reinforced Concrete (FRC) was explored to obviate the need for rebar
222 reinforcement in PCP members. Implementation of this concept was proposed via a modified
223 delivery system to print the fibers in such a way that their direction and placement are along
224 with the stress trajectory of PCP members. The prevalence and industrialization of PCP
225 members will be facilitated through the implementation of the proposed reinforcing methods
226 explored in this study.

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